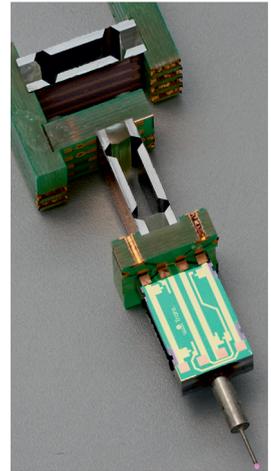
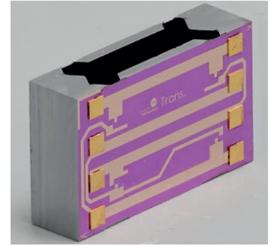
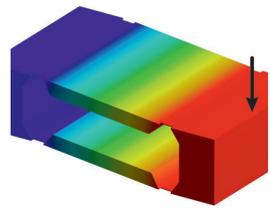


# 3D microprobe with isotropic serial kinematics for coordinate metrology

David Metz

Supervised by:  
Prof. Dr. rer. nat.  
Andreas Dietzel



Technische  
Universität  
Braunschweig

  
Institut für  
Mikrotechnik

# **3D microprobe with isotropic serial kinematics for coordinate metrology**

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der Technischen Universität Carolo-Wilhelmina zu Braunschweig

zur Erlangung der Würde  
eines Doktor-Ingenieurs (Dr.-Ing.)  
genehmigte

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## Preface and acknowledgment

The present PhD thesis is based on the results I achieved during my work as a research assistant at the Institute for Microtechnology (IMT) of the Technische Universität Braunschweig and in the Department 5.3 "Coordinate Metrology" of the Physikalisch-Technische Bundesanstalt (PTB) in the period from November 2013 to October 2019. Funding was provided by the German Research Foundation (DFG) within the framework of the transfer project "Dreiachsiger Mikrotaster mit isotropen mechanischen Eigenschaften zum Transfer in die industrielle Mikro-Koordinatenmesstechnik." The main results obtained during this project have been reported in peer review papers [1–4], at national and international conferences [5–9] and in patents [10, 11].

I would like to thank all people with whom I collaborated during this project. My special thanks go above all to my doctoral supervisor, Prof. Dr. rer. nat. Andreas Dietzel director of the IMT, who enabled me to work independently and under excellent technical conditions. Through his trustworthy care and support made a significant contribution to the success of this work.

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## Abstract

The remarkable developments in the field of micro- and nanofabrication in recent decades have been complemented by adapted new dimensional measurement techniques. Thus, the high demand for quality control of miniaturized components with high functional integration is met.

Tactile coordinate metrology has become a key technology to inspect 3D geometries in ranges from sub-micrometers up to meter sizes with high accuracy. With this purpose, workpiece surfaces are probed point by point in a coordinate measuring machine (CMM) using a probing system or probe. Micro-measurements are performed in special micro-CMMs with microprobes to allow the use of smaller probing elements, resulting in critical interactions with the workpiece. However, such devices are still only accessible to a few users.

Based on earlier investigations on membrane-based microprobes, a novel 3D microprobe design was developed to allow micro-measurements in conventional CMMs. Composed of three micro-fabricated measuring cells forming an isotropic serial kinematics, this microprobe offers a compact solution with an outer dimension of  $\varnothing$  11 mm. The parallelogram structure made of thin silicon hinges of the measuring cell allows large deflections of up to 600  $\mu\text{m}$  in all three directions and low probing forces  $< 30$  mN for 100  $\mu\text{m}$  deflections. These miniaturized load cells use piezoresistive sensors diffused into the silicon hinges to measure the deflection with sub-micrometer accuracy and resolution.

In this work, the novel and patented 3D microprobe design, its micro-fabrication, and a complete mechanical analysis are presented and discussed. Extensive characterization experiments confirmed the predictions of the theoretical analysis and provide design rules for also reaching future targeted properties of this novel class of microprobes. Finally, the successful integration and evaluation of the microprobe based on measurements of a gear standard in a CMM are reported, thereby opening up new possibilities for micro-probing in conventional CMMs.

**Keywords:** microprobe, silicon, piezoresistivity, micro-fabrication, isotropy, serial kinematics, coordinate metrology.



## Kurzfassung

Die Entwicklungen in der Mikro- und Nanofabrikation in den letzten Jahrzehnten wurden durch geeignete neue dimensionale Messverfahren ergänzt. So kann den hohen Anforderungen der Qualitätsprüfung von Miniaturbauteilen mit hoher Funktionsintegration nachgekommen werden.

Die taktile Koordinatenmesstechnik hat sich zu einer Schlüsseltechnologie entwickelt. 3D-Geometrien mit Submikrometern können so bis hin zu Metergrößen mit hoher Genauigkeit geprüft werden. Dabei erfolgt die punktweise Abtastung von Werkstückoberflächen in einem Koordinatenmessgerät (KMG) über ein Tastsystem. Mikromessungen werden in speziellen Mikro-KMGs mit Mikrotastern durchgeführt, um die Verwendung kleinerer Antastelemente zu ermöglichen. Jedoch sind solche Geräte nach wie vor nur wenigen Nutzern zugänglich.

Anhand vorheriger Arbeiten an membranbasierten Mikrotastern wurde ein neuartiger 3D-Mikrotaster für Mikromessungen in konventionellen KMGs entwickelt. Dieser besteht aus drei mikrogefertigten Messzellen, die eine isotrope serielle Kinematik bilden. Er bietet eine kompakte Lösung mit einem Außendurchmesser von 11 mm. Die Parallelogrammstruktur der Messzelle, die aus dünnen Silizium-Festkörpergelenken besteht, erlaubt große Auslenkungen von bis zu 600  $\mu\text{m}$  in allen drei Richtungen und geringe Antastkräfte  $< 30 \text{ mN}$  bei 100  $\mu\text{m}$  Auslenkung. Diese Miniaturkraftmesszellen verwenden in Siliziumgelenken eindiffundierte Piezowiderstände. So kann die die Auslenkung mit einer Genauigkeit und Auflösung im Submikrometerbereich ermittelt werden.

In dieser Arbeit werden der neuartige und patentierte 3D-Mikrotaster, dessen Mikrofertigung sowie eine vollständige mechanische Analyse vorgestellt und diskutiert. Umfangreiche Charakterisierungsexperimente bestätigten die theoretischen Vorhersagen und liefern Konstruktionsregeln, um in Zukunft gezielte Eigenschaften dieses neuartigen Mikrotasters zu erreichen. Schließlich wird über die erfolgreiche Integration und Evaluierung des Mikrotasters anhand von Messungen eines Verzahnungsnormals in einem KMG berichtet. Hierbei wird deutlich, dass sich neue Möglichkeiten für die Mikromessung in konventionellen KMGs eröffnen.

**Stichwörter: Mikrotaster, Silizium, Piezoresistivität, Mikrofabrikation, Isotropie, serielle Kinematik, Koordinatenmesstechnik.**



# Contents

<b>1</b>	<b>Introduction .....</b>	<b>1</b>
<b>2</b>	<b>State of the art in tactile micro-coordinate metrology.....</b>	<b>5</b>
2.1	Coordinate metrology .....	6
2.2	Tactile micro-coordinate metrology .....	9
2.2.1	Aspects of micro-probing .....	9
2.2.2	Micro-coordinate measuring machines .....	16
2.2.3	Micro-probing system .....	18
2.3	Recent developments on membrane microprobes .....	23
2.3.1	Membrane design for lower anisotropy.....	23
2.3.2	Stacked membrane design for lower anisotropy .....	24
2.4	The research gap to be closed .....	29
<b>3</b>	<b>State of the art of silicon micromechanics .....</b>	<b>33</b>
3.1	Silicon as construction and piezoresistive material .....	34
3.1.1	Silicon properties .....	34
3.1.2	Young's modulus of silicon .....	35
3.1.3	Piezoresistivity of silicon .....	39
3.2	Mechanical analysis of compliance mechanisms.....	43
3.2.1	Compliance matrix of a link.....	43
3.2.2	Compliance of serial and parallel structure of links .....	46
3.3	MEMS manufacturing techniques.....	48
3.3.1	Thin-film technologies.....	48
3.3.2	Micro structuring .....	48
3.3.3	Doping techniques .....	49
3.3.4	Bulk micromachining.....	50
3.3.5	Wafer bonding techniques.....	52
<b>4</b>	<b>Novel 3D microprobe based on isotropic serial kinematics.....</b>	<b>55</b>
4.1	Design and working principle of the novel microprobe .....	56
4.2	Micro-fabricated measuring cell .....	57
4.2.1	Design and working principle of the measuring cell.....	57
4.2.2	Wafer-level fabrication of the measuring cell.....	59
4.2.3	Interfacing of the measuring cell.....	68
4.2.4	Mechanical and sensing analysis of the measuring cell .....	69
4.3	Novel 3D isotropic microprobe .....	80
4.3.1	Assembly and contacting concept.....	80
4.3.2	Manufacture of the microprobe .....	81
4.3.3	Interfacing of the microprobe.....	84
4.3.4	Mechanical and sensing analysis of the novel 3D microprobe.....	88

<b>5</b>	<b>Experimental characterization.....</b>	<b>99</b>
5.1	Characterized micro-fabricated samples .....	100
5.2	Dimensions of measuring cell .....	101
5.3	Mechanical and sensing characterization .....	102
5.3.1	Experimental setup .....	102
5.3.2	Compliance of the measuring cell.....	103
5.3.3	Compliance of the microprobe .....	106
5.3.4	Working range.....	110
5.3.5	Sensitivity of the measuring cell.....	111
5.3.6	Sensitivities of the microprobe .....	114
5.4	Dynamic characterization .....	120
5.4.1	Experimental setup .....	120
5.4.2	Frequency response of the measuring cell.....	120
5.4.3	Frequency response of the microprobe .....	122
5.5	Signal stability and environmental influences .....	124
5.5.1	Noise and drift.....	124
5.5.2	Environment influences: temperature behaviour .....	125
<b>6</b>	<b>Integration and measurements in a CMM .....</b>	<b>129</b>
6.1	The P40 measuring machine.....	130
6.2	Mechanical and electrical interfaces .....	131
6.3	3D characterization of the microprobe.....	132
6.4	Evaluation of the microprobe in the P40 .....	136
6.4.1	Comparison and evaluation method.....	136
6.4.2	Determination of the measurement uncertainty.....	137
6.4.3	Probing repeatability.....	139
6.4.4	Measurement of a cube and a sphere .....	140
6.4.5	Measurement of a micro-gear measurement standard .....	143
6.4.6	Discussion of the evaluation of the microprobe .....	146
<b>7</b>	<b>Conclusion and outlook.....</b>	<b>147</b>
<b>8</b>	<b>Literature .....</b>	<b>155</b>
<b>Appendix A</b>	<b>Additional formulas for mechanical analysis.....</b>	<b>173</b>
<b>Appendix B</b>	<b>Additional figures and tables .....</b>	<b>191</b>
<b>Appendix C</b>	<b>Measuring cell fabrication process.....</b>	<b>197</b>

## List of symbols and abbreviations

Symbol (latin)	Unit	Explanation
$a$	Å	Lattice specific length
$a$	mm	Oscillations amplitude
$a_{CMM}$	$m \cdot s^{-2}$	Acceleration
$A$	-	Anisotropy
$A$	$Mm^2$	Area
$CM$	$mm \cdot V^{-1}$	Conversion matrix
$c_{ij,kl}, c_{ij}$	Pa or $N \cdot m^{-2}$	Elastic constants
$C, C_{ij}$	$mm \cdot N^{-1}$	Compliance
$d$	mm	Deflection
$d_t$	mm	Tip diameter
$d_i^Y, d_i^Z$	mm	Microprobe dimension
$E_n$	-	Proficiency test score
$E_F$	$V \cdot V^{-1} \cdot N^{-1}$	Force sensitivity
$E_u$	$V \cdot V^{-1} \cdot mm^{-1}$	Deflection sensitivity
$E$	Pa or $N \cdot m^{-2}$	Young's modulus
$E_{0,MPE}$	m	maximum permissible error
$f_{H\alpha}, f_{T\alpha}, F_\alpha$	m	Profile slope, form and total deviation
$f_{H\beta}, f_{T\beta}, F_\beta$	m	Helix slope, form and total deviation
$f, f_0$	Hz	Frequency, eigenfrequency
$F$	N	Forces
$G$	Pa or $N \cdot m^{-2}$	Shear modulus
$G_i$	-	Transformation matrix of change of basis
$h$	mm	Height or thickness
$I$	A	Current
$I_y, I_z$	$mm^4$	Second moments of inertia
$J$	$mm^4$	Torsional moments of inertia
$J_{ui}$	-	Transformation matrix of deflections
$J_{Li}$	-	Transformation matrix of loads
$k$	-	Coverage factor
$K, K_{ij}$	$N \cdot m^{-1}$	Stiffness
$K$	-	K-Factor of piezoresistive materials
$l, L$	mm	Length
$L$	-	Loads vector
$l_i, m_i, n_i$	-	Direction cosines
$m$	kg	Mass
$M$	$N \cdot m$	Torsional and Bending, moment

## List of symbols and abbreviations

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$N$	$\text{cm}^{-3}$	Dopant concentration
$p$	$\text{Pa}$ or $\text{N}\cdot\text{m}^{-2}$	Contact pressure
$P$	-	Probability
$P$	-	Piezoresistive correcting factor
$r$	$\text{m}$	Radius
$R$	$\Omega$	Resistance
$R_i$	-	Rotation matrix of change of basis
$R$	-	Resonance function
$s_{ij,kl}, s_{ij}$	$\text{Pa}^{-1}$ or $\text{m}\cdot\text{N}^{-2}$	Elastic coefficients
$s$	-	Experimental standard deviation
$T$	$^{\circ}\text{C}$ or $\text{K}$	Temperature
$T_E$	-	Euler's rotation matrix
$u$	$\text{m}$	Deflection
$u$	-	Measurement uncertainty
$U$	-	Extended measurement uncertainty
$U$	$\text{N}\cdot\text{m}$ or $\text{J}$	Energy of strain
$U_e$	$\text{V}$	Wheatstone bridge excitation voltage
$U_{si}$	$\text{V}$	Sensors output signals
$\nu, \nu_i, \nu_{ij}$	-	Poisson's ratio
$v$	$\text{m}\cdot\text{s}^{-1}$	Speed
$V_i$	-	Verification/correction matrix
$w$	$\text{m}$	Body width

<b>Symbol (greek)</b>	<b>Unit</b>	<b>Explanation</b>
$\alpha, \beta, \gamma$	$\text{rad}$	Euler's angles
$\delta$	$\text{m}$	Deformation depth
$\delta_{ovt}$	$\text{m}$	Over-travel
$\varepsilon$	$\text{m}$	Parasitic displacement error
$\varepsilon, \varepsilon_{ij}$	%	Mechanical strain
$\varepsilon_{lin}$	%	Linearity error
$\theta$	$\text{rad}$	Azimuthal angles
$\mu_s$	-	Friction coefficient
$\pi_{rq}, \Pi$	$\text{Pa}^{-1}$ or $\text{m}\cdot\text{N}^{-2}$	Piezoresistive coefficient, -matrix
$\rho$	$\Omega\cdot\text{m}$	Resistivity
$\sigma, \sigma_{ij}$	$\text{Pa}$ or $\text{N}\cdot\text{m}^{-2}$	Mechanical stress
$\sigma_{0.2}$	$\text{Pa}$ or $\text{N}\cdot\text{m}^{-2}$	Yield strength
$\sigma_F$	$\text{Pa}$ or $\text{N}\cdot\text{m}^{-2}$	Fracture stress
$\varphi$	$\text{rad}$	Oscillations phase
$\varphi$	$\text{rad}$	Elevation angles

<b>Abbreviation</b>	<b>Explanation</b>
CBA	Compliance based analysis
CMM	Coordinate measuring machine
EMC, EMI	Electromagnetic compatibility, interference
FEA, FEM	Finite element analysis, method
IMT	Institute of microtechnology, TU Braunschweig
ISO	International Organization for Standardization
IP	Interposers parts
KOH	Potassium hydroxide
MEMS	Microelectromechanical systems
METAS	Swiss Federal Institute of Metrology (Switzerland)
NMI	National measurement institute
NPL	National physical laboratory (United Kingdoms)
PCB	Printed circuit board
PDMS	Polydimethylsiloxane
PI	Polyimide
PTB	Physikalisch-Technische Bundesanstalt (Germany)
RIE, DRIE	Reactive-ion etching, Deep reactive-ion etching
SOI	Silicon on isolator