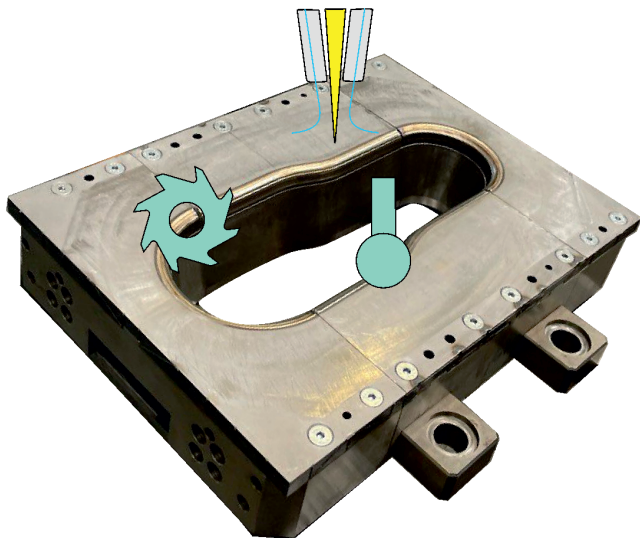
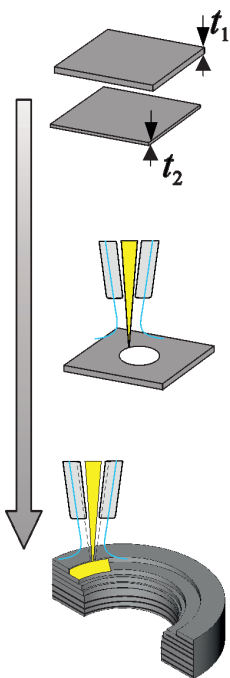


Hamed Dardaei Joghan

Hybrid additive manufacturing of metal laminated forming tools



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Vorsitzender der Prüfungskommission: PD Dr. habil. Tobias Kaiser

Berichter: Prof. Dr.-Ing. A. Erman Tekkaya

Mitberichter: Prof. Dr.-Ing. Jan T. Sehart

Prof. PD Dr.-Ing. Andreas Zabel

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Dormund, Febraury 2024

To my parents

Abstract

This thesis introduces and investigates a new resource-efficient manufacturing method for rapid tooling. The presented hybrid method combines two additive manufacturing processes: sheet metal lamination and direct energy deposition (DED). In this combination, the core of the forming tool is fabricated by sheet lamination in a short time and at a low cost. The resulting step areas are compensated by laser metal deposition (LMD), which is a subset of the DED process. Three post-processing methods, milling, ball burnishing and laser polishing, are applied and compared to improve the surface roughness of the deposited areas.

The results show the essence of the two-step filling strategy, in which a bonding step should bond together the tool sheets, and in the next step, the remaining stair-step areas should be filled by LMD. The tensile strength of the fillet bonding for different process parameters and tool sheet combinations shows that the higher laser power and feed rate result in higher strength; however, the sheet thickness also needs to be considered to avoid the melt-through of the thin sheets. In the filling step, filling in the radius direction shows better surface roughness, but the nozzle life is shorter. The preheating of the die sheet to reduce the residual tensile stress shows only a 25 % reduction, which causes waviness of the deposited surface. Therefore, it can be neglected.

A semi-analytical model to analyze the stress distribution showed the possibility of using the low-strength tool sheets in a major part of the laminated tool. Deep drawing experiments are successful for two types of blanks. The wear test study shows low wear of the dies manufactured by the hybrid method in comparison with the conventional method. The feasibility of manufacturing complex geometries is demonstrated by a manufactured demonstrator.

The economic and technological advantages of the hybrid method are compared with conventional and fully manufactured tools by LMD, and the number of possible sheet combinations for tool lamination is reduced by considering cost and energy criteria.

Zusammenfassung

In dieser Arbeit erfolgt die Entwicklung und Untersuchung eines neuen ressourceneffizienten Fertigungsverfahrens für das Rapid Tooling. Das vorgestellte Verfahren Tooling kombiniert zwei additive Fertigungskategorien: Sheet lamination und Direct Energy Deposition (DED). In dieser Kombination wird der Kern des Umformwerkzeugs durch Blechlaminierung in kurzer Zeit und zu geringen Kosten hergestellt. Die entstehenden Treppenstufenbereiche werden durch Laserpulvarauftragschweißen (LPA), zugehörig zur DED-Kategorie, kompensiert. Drei Nachbearbeitungsmethoden, Fräsen, Glattwalzen und Laserpolieren, werden zur Verbesserung der Oberflächenrauheit der aufgebrachten Flächen eingesetzt und verglichen.

Die Ergebnisse zeigen, dass das Konzept einer zweistufigen Füllstrategie, bei der die Werkzeugbleche zunächst zusammengefügt wurden, und im nächsten Schritt die verbleibenden Treppenstufenbereiche durch LPA gefüllt werden, von Vorteil ist. Untersuchungen an Kehlnahtverbindungen bei verschiedenen Prozessparametern und Werkzeugblechkombinationen zeigen, dass eine höhere Laserleistung und Vorschubgeschwindigkeit zu einer höheren Festigkeit führen; allerdings sollte auch die Blechdicke berücksichtigt werden, um das Durchschmelzen der dünnen Bleche zu vermeiden. Beim Füllen zeigt sich, dass ein Auffüllen in radialer Richtung eine bessere Oberflächenrauheit als Auffüllung in der Kehlnahtrichtung aufweist. Die Vorwärmung des Werkzeugblechs zur Verringerung der Zugeigenspannungen führt nur zu einer Verringerung um 25 %, was zu einer Welligkeit der aufgebrachten Oberfläche führt. Daher kann sie vernachlässigt werden.

Ein semi-analytisches Modell zur Analyse der Spannungsverteilung zeigt die Möglichkeit der Verwendung von Werkzeugblechen mit niedriger Festigkeit in einem Großteil des laminierten Werkzeugs. Tiefziehversuche sind für zwei Arten von Blechen erfolgreich, für kaltgewalzten hochfesten Stahl (HC380LA) und für eine Spezieltiefziehgüte (DC06). Verschleißuntersuchungen zeigen, dass der Verschleiß der mit der Hybridmethode hergestellten Matrizen im Vergleich zur konventionellen Methode gering ist. Ein Demonstrator beweist die Herstellbarkeit auch komplexer Geometrien.

Die wirtschaftlichen und technologischen Vorteile des Hybridverfahrens werden mit konventionellen und vollständig mit LMD gefertigten Werkzeugen verglichen und die Anzahl der möglichen Blechkombinationen für die Werkzeugauslegung wird unter Berücksichtigung von Kosten- und Energiekriterien reduziert.

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Publication of contents

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Surav Tank, 2023. Investigation of laser polishing and ball burnishing effects on laser metal deposited surfaces. Project work.

Formula symbols and abbreviations

Nomenclature

Symbol	Unit	Description
A	mm ²	Area
A_c	mm ²	Material mixture area with substrate after deposition
A_D	mm ²	Deposited area
A_g	-	Fracture strain
A_P	mm ²	Part's area
A_s	mm ²	Scrap's area
a	mm	Free length of the tool sheet
a_b	mm	Length of stacked beam under support
a_e	mm	Radial depth of cut
a_p	mm	Axial depth of cut
b	mm	Width of the tool sheet
b_s	mm	Tool sheet offset
c_d	mm	Clearance between the die and the punch
C	-	Constant value
C_L	mm	Cutting length
c	-	Thickness-to-length ratio
D	N	Axial stiffness of stacked beam
D_B	mm	Blank initial diameter
D_{Die}	mm	Inner diameter of deep drawing die
D_P	mm	Punch diameter
d	mm	Cylindrical hole with diameter
d_L	mm	Laser spot diameter

Symbol	Unit	Description
$\dot{D}$	g/min	Deposition rate
E	MPa	E-Module
E_B	J	Energy for ball burnishing
E_{Bulk}	J	Energy for production of bulk material
E_H	J	Energy for hardening
E_{LC}	J	Energy for laser cutting
E_{LMD}	J	Energy for LMD
E_{LP}	J	Energy for laser polishing
E_M	J	Energy for milling
E_{Powder}	J	Energy for production of powder
E_{PP}	J	Energy for post-processing
E_{Sheet}	J	Energy for production of sheet
E_{rq}	J	Required energy consumption
F_H	N	Horizontal force
f	mm/min	Feed rate or scanning speed
f_P	mm/min	Feed rate of laser polishing
G	GPa	Shear modulus
H	mm	Height of elastic support
H_B	RC or Vickers	Hardness
H'_B	-	Change of hardness
h_c	mm	Depth or height of the cup
h_d	mm	Hatching distance
I	mm ⁴	Inertia of moment
j	-	Degree of polynomial

Symbol	Unit	Description
k	GPa	Elastic modulus of elastic bed
L	-	Constant value
M	N.mm	Bending moment
m	-	Slope of the inter-planer spacing to different tits
m_p	kg	Part's mass
m_s	kg	Scrap's mass
m_{Step}	kg	Sum of stair-step areas
$\dot{m}$	g/min	Powder feed rate or mass flow
n	-	Number of stacked tool sheets
P	W	Laser power
P_{BH}	MPa	Blank holder pressure
P_N	-	Number of possible sheet combinations
P_P	W	Laser power for laser polishing
P_r	MPa	Reaction pressure of elastic bed
q	N/mm	Distributed force
$\underline{Q}$	N	Shear force in beam theory
$\bar{Q}$	mm ³ /h	Material removal rate
R	mm	Die corner radius
R'_m	mm	Bending radius after unloading
R'_a	-	Change of average surface roughness
R'_z	-	Change of maximum height of surface roughness
R_a	μm	Arithmetical mean deviation of the profile in 2D
R_m	MPa	Ultimate strength

Symbol	Unit	Description
R_m	mm	Bending radius before unloading
R_P	mm	Punch corner radius
$R_{p0,2}$	N·mm ⁻²	Tensile strength
R_z	μm	Maximum height of the profile in 2D
r	-	Anisotropy coefficient
r_n	-	Normal anisotropy
Δr	-	Planer anisotropy
S	N.mm ²	Stiffness of stacked beam
S_a	μm	Arithmetical mean deviation of the profile in 3D
SEC	J/kg	Specific energy consumption
S_k	μm	Roughness depth of the core
S_{mr}	%	Areal material ratio
S_z	μm	Maximum height of the profile in 3D
s	mm	Thickness position
T	°C	Temperature
T_s	mm	Sum of the stacked beam thicknesses
T_H	s	Time for hardening
T_{LC}	s	Time for laser cutting
T_{LMD}	s	Time for LMD
T_{PP}	s	Time for post-processing
T_T	s	Total manufacturing time
t	mm	Tool sheet thickness
t_b	mm	Blank thickness
u	mm	Displacement of the stacked beam

Symbol	Unit	Description
u'	rad	1 st order invariant of displacement (Bending angle)
u''	1/mm	2 nd order invariant of displacement
u_2'''	1/mm	3 th order invariant of displacement
V	mm ³	Volume
v_p	mm/min	Punch velocity
W_a	μm	Waviness arithmetical mean deviation of the profile in 3D
W_D	mm	Working distance between laser nozzle and deposited surface
X	-	Material yield
x^N	-	Normalized length in the x -direction
z^*	mm	Distance of the neutral layer to the middle of the beam layer's cross-section
z^N	-	Normalized length in the thickness direction
β	-	Deep drawing ratio
Γ	-	Coefficient factor
γ	$^\circ$	Angle
$\bar{\varepsilon}_{Plastic}$	-	Equivalent plastic strain
ε	-	Strain
θ	W/(kg/mm)	Track-specific power density
θ_z	$^\circ$	Angle of rotation of normal to the mid- surface of the deflection in beam theory
Λ	-	Correction factor for maximum von Mises stress
λ	J/mm	Applied energy per unit length by laser polishing

Symbol	Unit	Description
μ	-	Friction factor
ρ	Kg/mm ³	Density
$\sigma_{v.M.}^N$	-	Normalized von Mises stress
σ_f	MPa	Flow stress
σ_n	MPa	Normal stress
σ_r	MPa	Radial stress
σ_t	MPa	Tangential stress
σ_w	MPa	Weld fracture strength
τ	MPa	Shear stress
ν	-	Poisson's ratio
$\emptyset$	-	Dilution ratio

Indices

Index	Description
0	Initial value
eff	Effective
eq	Equivalent
max	Maximum
min	Minimum

Abbreviations

Abbreviation	Description
2D	Two dimensional
3D	Three dimensional
AM	Additive manufacturing
AWJ	Abrasive water jet
BC	Boundary condition
CAD	Computer-aided design
CAM	Computer-aided manufacturing
CIRP	International academy for production engineering
CNC	Computer numerical control
CVD	Chemical vapour deposition
DED	Direct energy deposition
EBSD	Electron backscatter diffraction
EDX	Energy-dispersive X-ray spectroscopy
FEM	Finite element method
FGM	Functionally graded material
FSW	Friction stir welding
GMAW	Gas metal arc welding

GTAW	Gas tungsten arc welding
HAM	Hybrid additive manufacturing
HAZ	Heat affected zone
LBMD	Laser-based metal deposition
LDMD	Laser direct metal deposition
LENS	Laser engineered net shape
LFF	Laser freeform fabrication
LLM	Layer laminated manufacturing
LMD	Laser metal deposition
LMDS	Laser metal deposition shaping
LOM	Laminated object manufacturing
LSA	Laser surface alloying
LST	Laminated steel tooling
N.A.	Neutral axis
PEL	Profiled edge laminae
RT	Room temperature
SEC	Specific energy consumption
SOM	Surface over-melt
SSM	Shallow surface melting
TIG	Tungsten inert gas